

# **AN-1081 A Low Cost, Low Parts-Count DC/DC Converter With Multiple Outputs**

## **ABSTRACT**

This application report describes a simple low cost, low parts-count multiple output DC/DC converter based on the LM2596 five terminal step-down switching regulator. The circuit described provides multiple output voltages (positive and negative) with good regulation using a step-down converter circuit with flyback windings. It uses only one switching regulator IC.

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## **1 Performance**

The circuit has an input voltage range of 15 V to 40 V. It has 5 outputs: 3.3 V at 1.5A; +12 V and –12 V at 50 mA each; and +5 V and –5 V at 50 mA each. The 3.3 V, +5 V and –5 V outputs are regulated with  $\pm 5\%$  accuracy over line and load variations. The +12 V and –12 V outputs are regulated with  $\pm 20\%$  accuracy. A typical application of this circuit is where the 3.3 V output provides the power to the main circuit that is 3.3 V logic, the  $\pm 5$  V outputs power the 5 V logic and  $\pm 12$  V outputs provide the bias supply of op-amps.

The efficiency of the circuit with full load at all outputs is 75%. The ripple voltage across the 3.3 V output is less than 20 mV and that across the  $\pm 12$  V outputs is less than 30 mV. The ripple across the  $\pm 5$  V is less than 10 mV.

## 2 Schematic and Parts List

Figure 1 shows the schematic of the circuit.

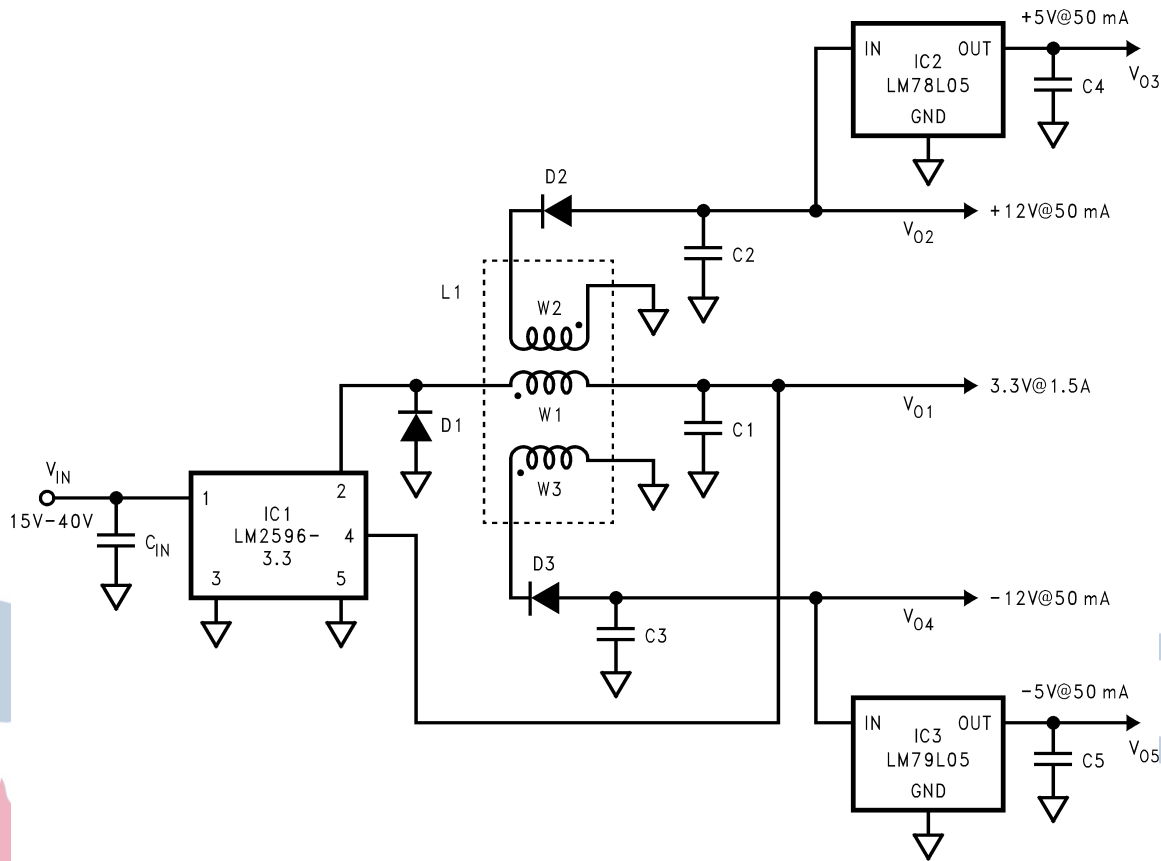


Figure 1. Circuit Schematic

The parts list for the circuit is:

Cin : 220  $\mu$ F, 50 V, Nichicon UPL1H221MPH,

C1: 270  $\mu$ F, 63 V, Nichicon UPL1J271MRH,

C2, C3: 47  $\mu$ F, 35 V, Nichicon UPL1V470MPH,

D1: MBR360,

D2, D3: 1N459,

C4, C5: 0.01  $\mu$ F,

IC1: LM2596-3.3 ( SIMPLE SWITCHER® Step-Down Voltage Regulator),

IC2, IC3: LM78L05, and LM79L05. (3- Terminal Regulators),

L1: Custom Inductor with three windings (W1, W2 and W3) with the following specs:

**W1**:— 47  $\mu$ H; Peak Current: 2.6A, RMS Current  $\approx$  2.32A

**W2**:— Number of turns = 3.4 x Number of turns in W1; RMS Current; 113 mA

**W3**:— Same as W2.

### 3 Circuit Operation

The circuit operates as a standard step-down (buck) switching regulator, except for the flyback windings (W2, W3). The flyback windings conduct current during the on-period of D1 and supply the 3-terminal regulators (IC2 and IC3). C2 and C3 should be of high enough value to smooth out the high ripple due to the flyback action of W2 and W3. The flyback windings supply the +12 V and -12 V outputs with  $\pm 20\%$  accuracy. The 3-terminal regulators are used to provide +5 V and -5 V with  $\pm 5\%$  accuracy. The LM2596 regulates the main output (3.3 V) by standard step-down action.

### 4 Design

#### 4.1 Step 1: Design of Step-Down Regulator for the Main (3.3 V) Output

This can be done using the *Switchers Made Simple* software by Texas Instruments. The following values (underlined>) are entered into the software:

$V_{IN}(\text{min})$ : 15 V

$V_{IN}(\text{max})$ : 40 V

$V_{OUT}$ : 3.3 V

$I_{OUT}$ :

$$I_{OUT} = I_{O1} + N (I_{O2} + I_{O3} + I_{O4} + I_{O5}) \quad (1)$$

1.5A is the load for the 3.3 V output.  $I_{O1}$ ,  $I_{O2}$ ,  $I_{O3}$ ,  $I_{O4}$  and  $I_{O5}$  are the load currents of outputs  $V_{O1}$ ,  $V_{O2}$ ,  $V_{O3}$ ,  $V_{O4}$  and  $V_{O5}$ , respectively. N is the turns ratio between W2 and W1 (also between W3 and W1). It is calculated using:

$$N = \frac{V_{O2} + V_{FD2}}{V_{O1} + V_{FD1}} = \frac{12 + 0.7}{3.3 + 0.4} = 3.4 \quad (2)$$

In this equation,  $V_{FD2}$  is the forward voltage drop of D2 and  $V_{FD1}$  is the forward voltage drop of D1.

Using Equation 2,  $I_{OUT} = 1.5A + 3.4 (50 \text{ mA} + 50 \text{ mA} + 50 \text{ mA} + 50 \text{ mA}) = 2.18A$

$I_{OUT} = 2.18A$ .

The software designs the step-down regulator and gives the following values:

IC1: LM2596-3.3

$C_{IN}$  : 220  $\mu\text{F}$ , 50 V, Nichicon UPL1H221MPH

C1: 270  $\mu\text{F}$ , 63 V, Nichicon UPL1J271MRH

D1: MBR360

L1: 47  $\mu\text{H}$ .

IC  $I_{pk}$ : 2.38A.

$C_{IN}$  and  $C_1$  have been chosen primarily for ESR, not for voltage rating.

## 4.2 Step 2: Design OF L1 and Flyback Outputs

### 4.2.1 Design of L1

The value of inductance due to W1 is the same as the value of L1 obtained in Step 1. The number of turns in windings W2 ( $N_{w2}$ ) and W3 ( $N_{w3}$ ) are

$$\begin{aligned} N_{w2} &= N_{w3} = N \times \text{Number of turns in W1} \\ &= 3.4 \times \text{Number of turns in W1.} \end{aligned} \quad (3)$$

The peak current in W2 ( $I_{pkw2}$ ) is:

$$\begin{aligned} I_{pkw2} &= \frac{I_{O2} + I_{O3}}{1 - \frac{V_{O1}}{V_{in(min)}}} \\ &= \frac{0.05+0.05}{1 - \frac{3.3}{15}} = 128 \text{ mA.} \end{aligned} \quad (4)$$

The peak current in W3 ( $I_{pkw3}$ ) is:

$$\begin{aligned} I_{pkw3} &= \frac{I_{O4} + I_{O5}}{1 - \frac{V_{O1}}{V_{in(min)}}} \\ &= \frac{0.05+0.05}{1 - \frac{3.3}{15}} = 128 \text{ mA.} \end{aligned} \quad (5)$$

The RMS current of W2 ( $I_{rmsw2}$ ) is:

$$\begin{aligned} I_{rmsw2} &\approx \sqrt{I_{pkw2}^2 \left(1 - \frac{V_{O1}}{V_{in(min)}}\right)} \\ &= \sqrt{0.128^2 \left(1 - \frac{3.3}{15}\right)} = 113 \text{ mA.} \end{aligned} \quad (6)$$

The RMS current of W3 ( $I_{rmsw3}$ ) is:

$$\begin{aligned} I_{rmsw3} &\approx \sqrt{I_{pkw3}^2 \left(1 - \frac{V_{O1}}{V_{in(min)}}\right)} \\ &= \sqrt{0.128^2 \left(1 - \frac{3.3}{15}\right)} = 113 \text{ mA.} \end{aligned} \quad (7)$$

The peak current of W1 ( $I_{pkw1}$ ) is:

$$\begin{aligned} I_{pkw1} &\approx I_C I_{pk} + 3.4 (I_{pkw2} - (I_{O2} + I_{O3}) + I_{pkw3} - (I_{O4} + I_{O5})) \\ &= 2.38\text{A} + 3.4 (0.128 - (0.05 + 0.05) + (0.05 + 0.05)) = 2.6\text{A.} \end{aligned} \quad (8)$$

This value is below the  $I_{CL(min)}$  specified in the *LM2596 SIMPLE SWITCHER® Power Converter 150 kHz 3A Step-Down Voltage Regulator Data Sheet* ([SNVS124](#)) and, thus, is acceptable.

Since the current through W1 is continuous the RMS current is approximately equal to  $I_C I_{pk}$ , which is 2.38A.

### 4.2.2 Selection of C2 and C3

C2 and C3 should be selected to be large enough to smooth out the high ripple caused due to the flyback operation of W2 and W3. Also they should have a low enough ESR value. 47  $\mu\text{H}$ , 50 V aluminum electrolytic capacitors are sufficient for this design.

### 4.2.3 Selection of D2 and D3

D2 and D3 should be selected to conduct the sum of the current through the two outputs each is connected to. The DC blocking voltage rating of D2 ( $V_{RD2}$ ) and D3 ( $V_{RD3}$ ) are calculated using equations (9) and (10).

$$\begin{aligned} V_{RD2} &= (V_{in(max)} - V_{O1})N + V_{O2} & (9) \\ &= (40\text{ V} - 3.3\text{ V}) \times 3.4 + 12\text{ V} = 137\text{ V}. \end{aligned}$$

$$\begin{aligned} V_{RD3} &= (V_{in(max)} - V_{O1})N + V_{O3} & (10) \\ &= (40\text{ V} - 3.3\text{ V}) \times 3.4 + 12\text{ V} = 137\text{ V}. \end{aligned}$$

1N459 diodes that have a reverse voltage rating of 175 V are used in this design.

### 4.3 Step 3: Design of 3-Terminal Regulators

The 3-terminal linear regulators are used to regulate the auxiliary outputs with  $\pm 5\%$  accuracy. Their design is straightforward and can be done using the data sheets for the 3-terminal regulators.

## 5 Advantages

This circuit can save both parts and cost by making use of only one step-down regulator IC, two inexpensive 3-terminal linear regulators, and a simple three-winding inductor to provide 5 outputs.

The usual solution for this design with multiple (positive and negative) outputs is a flyback converter. The design described in this application report is better than using a flyback regulator with multiple outputs because:

- It uses a much smaller output capacitor for the 3.3 V output (270  $\mu\text{F}$  against 2.4 mF for flyback solution with a comparable output ripple voltage).
- It uses an inductor with only three windings whereas a flyback regulator solution requires a transformer with four windings.
- The overall peak current of the inductor in this design is less than that of a flyback transformer for the same application.
- Transformer construction is simplified because the leakage inductance does not result in power loss. Because of these reasons the magnetic structure of this design costs less than that in a flyback converter design.
- The peak switch current of this design is much less than that of a similar flyback design. The disadvantages of this design compared to the flyback converter are
- The 3.3 V output should be loaded to keep the inductor in continuous conduction mode. Otherwise large peak currents result in the flyback windings. In worst cases (deep into discontinuous conduction mode), the auxiliary outputs ( $\pm 12\text{ V}$  and  $\pm 5\text{ V}$ ) will not be regulated.
- When the duty cycle of the main output gets large, large peak currents result in the flyback windings and may result in loss of regulation of the auxiliary outputs in worst cases.
  - In most applications the advantages far outweigh the disadvantages, as can be inferred from the comparison above.
  - The IC's used in this circuit are all available in surface mount packages.

## 6 Summary

In applications where multiple output DC/DC conversion is needed, the circuit presented in this application report is an attractive solution. It is low cost, has a low-parts count, and provides the regulation needed with good efficiency. The detailed design procedure given in this document makes this design easy and straightforward.

## 7 References

*LM2596 SIMPLE SWITCHER® Power Converter 150 kHz 3A Step-Down Voltage Regulator Data Sheet*  
([SNVS124](#))

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